# Study of the Vickers hardness and corrosion behavior of experimental Ti-Mo alloy in dental office bleaching agents

*Estudo da dureza Vickers e comportamento de corrosão da liga experimental Ti-Mo em agentes clareadores para uso em consultório* 

*Estudio de la dureza Vickers y comportamiento de corrosión de la aleación experimental Ti-Mo en agentes blanqueadores para uso en consultorio* 

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### Abstract

At present, titanium and its alloys stand out for their mechanical and biological properties. Vickers hardness and the effect of 15%, 22% and 35% hydrogen peroxide ( $H_2O_2$ ) on Ti-10Mo alloy corrosion were evaluated. A conventional double-walled glass cell was used for thermostatization. As reference electrode was used the Ag/AgCl (s)/KClsat and as auxiliary electrode graphite stick. The work electrodes consisted of Ti-10Mo cylinders embedded in polyethylene, with electrical contact by brass wire and silver paint on one end. The electrolyte used was  $H_2O_2$  in concentrations of 15%, 22% and 35% and potentiodynamic measurements were recorded. The Vickers hardness was evaluated before the treatment using Vickers penetrator under load of 1000g and dwell time of 10s / measurement separately. The results showed an increase in the corrosion values in direct relation with the increase of the  $H_2O_2$  concentrations of 15% and 22% the results showed a tendency to pseudopassivation, with release of TiO<sub>2</sub> and part of the product of the corrosion becoming semi-adherent to the surface of the working electrode and another part passing through the middle, characterizing intermediate corrosion velocity. It was concluded that higher  $H_2O_2$  concentrations produced higher electrode activity.

Descriptors: Titanium; Alloys; Surface Properties; Corrosion; Tooth Bleaching Agents.

#### Resumo

Na atualidade, titânio e as suas ligas se destacam por suas propriedades mecânicas e biológicas. Avaliou-se a dureza Vickers e o efeito do peróxido de hidrogênio ( $H_2O_2$ ) a 15%,22% e 35% na corrosão da liga Ti-10Mo. Utilizou-se célula convencional de vidro de parede dupla para a termostatização. Como eletrodo de referência foi empregado o Ag/AgCl<sub>(s)</sub>/KCl<sub>sat</sub> e como eletrodo auxiliar bastão de grafite. Os eletrodos de trabalho consistiram de cilindros de Ti-10Mo embutidos em polietileno, com contato elétrico por fio de latão e tinta de prata em uma das extremidades. O eletrólito utilizado foi  $H_2O_2$  em concentração de 15%, 22% e 35% e medidas potenciodinâmicas foram registradas. A dureza Vickers foi avaliada antes do tratamento utilizando penetrador Vickers sob carga de 1000g e tempo de permanência de 10s/medição separada. Os resultados obtidos mostraram aumento nos valores de corrosão em relação direta com o aumento da concentração de  $H_2O_2$ . Na concentração de 35%, em corrente constante de ~1.0V a liga não passivou, caracterizando alta taxa de corrosão. Nas concentrações de 15% e 22% os resultados apontaram tendência à pseudopassivação, com liberação de TiO<sub>2</sub> e parte do produto da corrosão tornando-se semiaderente à superfície do eletrodo de trabalho e outra parte passando para o meio, caracterizando velocidade de corrosão intermediária. Concluiu-se que maiores concentrações de  $H_2O_2$  produziram maior corrosão eletroquímica. **Descritores:** Titânio; Ligas; Propriedades de Superfície; Corrosão; Clareadores Dentários.

#### Resumen

En la actualidad, titanio y sus aleaciones se destacan por sus propiedades mecánicas y biológicas. Se evaluó la dureza Vickers y el efecto del peróxido de hidrógeno (H<sub>2</sub>O<sub>2</sub>) al 15%, 22% y 35% en la corrosión de la aleación Ti-10Mo. Se utilizó una célula convencional de vidrio de doble pared para la termostatización. Como electrodo de referencia se utilizó el Ag/AgCl (s /KClsat y como electrodo auxiliar bastón de grafito. Los electrodos de trabajo consistieron de cilindros de Ti-10Mo embutidos en polietileno, con contacto eléctrico por hilo de latón y tinta de plata en una de las extremidades. El electrolito utilizado fue  $H_2O_2$  en concentración del 15%, el 22% y el 35% y las medidas potenciodinámicas se registraron. La dureza Vickers fue evaluada antes del tratamiento utilizando penetrador Vickers bajo carga de 1000g y tiempo de permanencia de 10s / medición separada. Los resultados obtenidos mostraron un aumento en los valores de corrosión en relación directa con el aumento de la concentración de H<sub>2</sub>O<sub>2</sub>. En la concentración de 35%, en corriente constante de ~1.0V la aleación no pasivó, caracterizando alta tasa de corrosión. En las concentraciones de 15% y 22% los resultados apuntaron tendencia a la pseudopasivación, con liberación de TiO2 y parte del producto de la corrosión volviéndose semiadente a la superficie del electrodo de trabajo y otra

parte pasando hacia el medio, caracterizando velocidad de corrosión intermedia. Se concluyó que mayores concentraciones de H<sub>2</sub>O<sub>2</sub> produjeron mayor corrosión electroquímica.

Descriptores: Titanio; Aleaciones; Propiedades de Superficie; Corrosión; Blanqueadores Dentales.

## **INTRODUCTION**

Titanium and its alloys exhibit excellent mechanical properties as well as biocompatibility. This superior behavior makes titanium alloys suitable material for use in biomedical applications<sup>1-5</sup>. In the last decades, it was particular interest to develop  $\beta$  Ti-based alloys produced from non-toxic elements and that present lowest elasticity modulus and high strength such as Ti-Mo<sup>5-8</sup>.

Ho et al.<sup>9</sup> reported that both crystalline structure and microstructures of the Ti-Mo alloy is sensitive to their molybdenum contents. They showed that molybdenum content of 10wt% is sufficient for to stabilize  $\beta$ -phase at room temperature. Also 10% Mo microstructure offers excellent ductility and strength<sup>8</sup>. All the titanium alloys containing 7.5-20 wt% has higher values of bending

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strength and Ti-10Mo has the highest (1752 MPa). Bending strength of Ti-10Mo is twice that of c.p.Ti (884 MPa) and little lower than Ti-6Al-4V (1860MPa)<sup>9</sup>.

It's well recognized that the release of aluminum and vanadium ions from the Ti-6Al-4V alloy might cause health problems, such as neurologic disorders and osteomalacia<sup>10</sup>. The development of non-toxic element  $\beta$ -type Ti alloys, such as Ti-Mo<sup>6,8,11</sup>, Ti-Nb<sup>12-14</sup>, Ti-Zr<sup>15</sup> and Ti-Ta<sup>16-18</sup> had been increased.

To further develop the potential properties and promising applications Ti-10Mo alloy, in our previous study, we investigated the effect of commercial mouthwashes on the corrosion resistance and found that protective characteristics of this passive film are lower in fluoride mouthwashes<sup>1</sup>. The dissolution of the TiO<sub>2</sub> film may occur due oral electrolytic environmental conditions and could affect properties of materials such as microhardness<sup>1,19</sup>.

These conditions include tooth bleaching, one the most popular treatment on esthetic dentistry. Since 1989, the beginning of the teeth whitening idea<sup>20</sup> there was a rapid increase of the demand for dental whitening to satisfy high patient expectations, driven strongly by an enhanced awareness of beauty and esthetics $^{21}$ . There are many techniques available for this procedure such as in-office bleaching, at-home use of bleaching trays, strip-based materials, or a combination of the treatment methods<sup>22</sup>. Hydrogen peroxide (HP) is the active agent in-office dental bleaching materials<sup>22,23</sup>. Also is used combined with urea to form carbamide peroxide which it is applied in the at-home bleaching option. In an aqueous environmental the carbamide peroxide decomposes to release hydrogen peroxide: 10% carbamide peroxide yields roughly 3.5% hydrogen peroxide. High hydrogen peroxide concentration has been used as in-office bleaching materials (typically 20-38%) for whitening of vital teeth<sup>23</sup>. Investigators report adverse effects of bleaching on dental materials according treatment method and type or concentration of the active agent (hydrogen peroxide or carbamide peroxide). Al-Salehi et al.<sup>25</sup> founded that metal ion release from the Ni-Cr and Pd-Cu-Ga alloys increased with increasing hydrogen peroxide concentration (0 to 30%). Similar results founded at nickel-chromium dental alloys<sup>26</sup>. Takemoto et al.<sup>27</sup> believe that discoloration in titanium alloys (Ti-Pd, Ti-Al-V, Ti-Al-Nb, Ti-Ni, Ti-Cu and Ti-Cr) immersed in hydrogen peroxide-containing acidulated solutions is caused by an increase in the thickness of this oxide film, whereas discoloration of Ti-Ni is caused by corrosion.

In this study, the microhardness and corrosion behavior of experimental Ti-710Mo alloy in-office dental bleaching agents have been investigated.

## **MATERIAL AND METHOD**

The Ti-Mo alloy with 10 wt.% Mo was made by melting of commercially pure titanium (c.p.Ti) grade 1 and commercially pure molybdenum (99.9%) into one 15 g button (~1.3 cm diameter and ~2.6 cm length) in an argonarc melting furnace. The ingots were remelted ten times in order to improve chemical homogeneity. Cylinders (with cross-section of 1 cm<sup>2</sup>) were machined from ingots of Ti-Mo experimental alloy. These cylinders and c.p.Ti discs with 1.1 cm diameter were mounted in polyester resin and employed as working electrodes. Before each experiment, working electrodes were ground with 600 and 1200 grade emery papers, rinsed with distilled water and dried in air. The counter electrode

was a platinum wire and reference electrode was an Ag/AgCl, KCl saturated electrode. The open circuit potential measurements, potentiodynamic and chronoamperometric curves were performed by means of an EG&G PAR Potentiostat/Galvanostat Model 283 (PerkinElmer Instruments Inc., USA). The conventional three-compartment double wall glass cell was connected to a constant temperature circulator operating at  $37 \pm 0.5^{\circ}$ C to simulate mouth conditions The test solutions used in this study were the dental office bleaching agents: 15% hydrogen peroxide ( $H_2O_2$ ), 22% hydrogen peroxide ( $H_2O_2$ ) and 35% hydrogen peroxide  $(H_2O_2)$ . The assessment of individual effect of active ingredient was studied by using 0.05% sodium fluoride pH=6.0. Corrosion behavior was studied in naturally aerated conditions. Open circuit potential measurements were recorded during an immersion time of 8 h. Potentiodynamic polarization curves were recorded in electropositive direction at a sweep rate of 0.02 V/min starting from -1.00V up to 2.50V.

Vickers hardness measurements were recorded on Ti-10Mo disks(n=5) using a MHT-1 microhardness tester equipped with a Vickers indenter under a load of 1000g and with a dwell time of 10s for each separate measurement (Digital Microhardness Tester HMV-2T, Shimadzu, Japan). All values of the Vickers microhardness (Hv) were recorded along a randomly selected diameter of each disk. For be obtained a high degree of accuracy, the average values of Hv were determined at selected positions separated incrementally by distances of 0.3 mm along each diameter. At every point the average value of Hv was achieved from six separate hardness measurements recorded at points uniformly arrayed around the selected position and separated from this position by distances of 0.15 mm. These six separate measurements were used also to estimate the 95% error bars for each separate point. Vicker hardness measurements on c.p.Ti (n = 5) discs were obtained for comparative analysis.

# RESULTS

Vicker's microhardness measures were performed before corrosion behavior test. The hardness values for Ti-10Mo alloy samples were significantly higher (229,08  $\pm$ 3,39) than pure titanium (187  $\pm$  4), resulting from the solid solution hardening caused by the addition of molybdenum having a higher atomic mass than titanium.

The results of corrosion test show that the value of the open circuit potential tends to be more positive when the electrolyte concentration is higher. This can be explained by the fact that more concentrated solutions of hydrogen peroxide produce more stable species on the alloy surface or that such values are due to the variation of the electrolyte concentration over the Ti-Mo in the medium.

Figure 1 shows the curves obtained for Ti-10Mo immersed in hydrogen peroxide solution at the three naturally aerated study concentrations at 37  $^{\circ}$  C. Through this technique it was possible to determine the corrosion potential, which corresponds to the stabilization potential of the system.

It is observed that after 7 hours of immersion the potential is almost constant and corresponds to the potential provided by the spontaneous reactions that occur in the surface of the material in the electrolyte under study. In general, at the initial test time, a slight shift of the potential to nobler values occurs, and then a decrease of that potential, reaching a more negative value. Note that the titanium alloy in the H<sub>2</sub>O<sub>2</sub> solution at either 15%, 22% or

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35% concentration achieves stability after about 60 minutes of immersion.

In the first few minutes of immersion, the increase in open circuit potential may be associated with the decrease of the active area of the electrode by the growth of an oxide film on the alloy surface due to the oxidizing properties of the medium. The presence of compact films and insulation prevents the process of corrosion of the material, as they act as a barrier, making the material passive in the study medium. The result is an increase in the potential of the system. In the specific case of the Ti10Mo alloy in  $H_2O_2$ , the decrease of the potential in the first 60 minutes indicates that the film formed on the electrode is not very protective. The dissolution of the oxide or formed oxides and less noble constituents of the alloy results in the decrease of the potential and the stabilization thereof in values more negative than that of the instant of immersion of the electrode in the solution. The stabilization potential corresponds to the equilibrium potential of the species involved in the corrosion process.

The results show that the value of the open circuit potential tends to be more positive when the electrolyte concentration is higher. This can be explained by the fact that more concentrated solutions of hydrogen peroxide produce more stable species on the alloy surface or that such values are due to the variation of the electrolyte concentration over the Ti10Mo in the medium.



**Figure 1:** Potential measurements in open circuit with time for alloy in  $H_2O_2$  medium with different concentrations.

Figure 2 shows the results of the anodic potentiodynamic polarization tests obtained in 15%, 22% and 35% hydrogen peroxide solution performed immediately after 7 hours of open circuit immersion. It can be observed that the Ti-10Mo alloy in 15%  $H_2O_2$  solution has a current shoulder located at approximately + 0.64V, followed by a decrease in current, revealing a tendency to passivation of the material. When the potential reaches values greater than 1.2V the current showed increases

concentration studied the non-passive alloy. The displacement of the potential corresponding to current maxima; high values of anodic current indicate the participation of the electrolyte in the oxidation process and probably the presence of poor protective and porous films.



**Figure 2:** Anodic potentiodynamic polarization tests obtained in 15%, 22% and 35% hydrogen peroxide solution performed immediately after 7 hours of open circuit immersion.

In Figure 3 the potentiodynamic polarization curves of the alloy in naturally aerated H<sub>2</sub>O<sub>2</sub> solution were recorded at 0.020 V/min, with scanning starting at the cathode region, about -0.40 V below potential corrosion, in the potential directions positive. The cathodic region exhibits a current density where no limiting oxygen reduction current is observed at any of the concentrations under study. An increase in the cathodic current is observed clearly with the increase of the concentration of hydrogen peroxide. The Ti-10Mo alloy in the presence of 35%  $H_2O_2$  shows a higher cathodic current density, which is considerably high (~10-3 A cm-2). For the 15% and 22%  $H_2O_2$  solutions the current density is lower (about 10-4 A cm-2). This result confirms what was mentioned previously where the observed behavior can be attributed to the reduction of the electrolyte on the electrode. In the anodic region the behavior is analogous to that observed for the anodic curves obtained from the corrosion potential. When the tests are performed in a less concentrated solution of  $H_2O_2$ , the formation of less protective oxide can be observed.



again. This behavior is typical of a pseudopassive material, that is, the formed film is not very protective and even before the occurrence of passivation the rupture of the film occurs. The high current value indicates the presence of a porous film. The behavior of the alloy in 22%  $H_2O_2$  solution is similar. The oxidation current shoulder shifted to about + 0.74 V and the current decrease observed after the current shoulder is less pronounced. In 35%  $H_2O_2$  solution there is practically no current shoulder but only an increase in current reaching a constant value of approximately + 1.0V. The current value is quite high about 1.1 A cm-2. This behavior shows that in the range of hydrogen peroxide

**Figure 3:** Potentiodynamic polarization curves of the alloy in naturally aerated  $H_2O_2$  solution at 0.020 V / min.

A c.p.Ti polarization curve for comparison is shown in Figure 4. When the behavior of Ti10Mo and c.p.Ti in 22% H<sub>2</sub>O<sub>2</sub> solution is compared, the presence of maximum

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current, which can be attributed to the formation of an oxide film on the metal, is also verified in the anodic region. However the observed current is lower, which shows changes in the properties of the titanium oxide film formed from pure Ti and the Ti-10Mo alloy. As the current value for the alloy is higher, this may indicate the formation of film less protective than that formed from pure Ti or catalytic effect of molybdenum on the oxidation of hydrogen peroxide.



**Figure 4:** Potentiodynamic polarization curves for c.p.Ti (grade 1) and Ti-10Mo alloy in 22% H 2 O 2 solution at T37 ° C.

Table 1 presents the values of corrosion potentials and current density obtained at constant potential value (+0.70V) for Ti-10Mo alloy in the three media under study.

Table 1. Values of corrosion potentials and current density obtained

Ti-10Mo				
$H_2O_2$	E <sub>corr</sub> (V)	j (A cm⁻²)		
15%	- 0,78	3,5 x 10 <sup>-4</sup>		
22%	- 0,62	6,7 x 10 <sup>-4</sup>		
35%	- 0,33	1,1 x 10 <sup>-3</sup>		

Figure 5 shows the surface of Ti10Mo before corrosion test with peroxide hydrogen solutions. Figures 6-8 exhibit the surface of Ti10Mo after corrosion behavior  $H_2O_2$  at 22%, the best result among three peroxide hydrogen solutions.





**Figure 6:** Surface of Ti10Mo after corrosion behavior  $H_2O_2$  at 22%



Figure 7: Surface of Ti10Mo after corrosion behavior H<sub>2</sub>O<sub>2</sub> at 22%.



Figure 8: Surface of Ti10Mo after corrosion behavior  $H_2O_2$  at 22%.

#### DISCUSSION

The performance of Ti alloys intended to be used in orthopedic and dental devices is generally examined by mechanical and biological properties<sup>28</sup>.

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10 μm	EHT = 20.00 kV	Signal A = CZ BSD	I Probe = 348 pA	Aperture Size = 20.00 μm	LAIMat
H	WD = 8.5 mm	Mag = 1.00 K X	Spot Size = 460	Chamber = 2.24e-003 Pa	FEG-UNES

Figure 5: Surface of Ti10Mo before corrosion test

In the present paper, Vickers hardness means of Ti-10Mo was remarkably higher than that of the c.p. Ti which was attributed to the decreased grain size and the solid solution effect of alloying elements. It is know that the increase in Vickers hardness decreases the incidence of wear of biomedical material<sup>29</sup>. The results obtained were agreeing with results found by Ho et al.<sup>9</sup> that investigated structure and properties of a series of binary Ti-Mo alloys with molybdenum contents ranging from 6 to 20 wt%.

Although several studies have evaluated the effects of bleaching agents on the physicochemical properties of

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restorative materials, few investigators have studied the corrosion of titanium alloys when exposed to these products.

Takemoto et al.<sup>27</sup> suggest that although titanium has high resistance to corrosion, during clinical behavior in the oral environment it may experiment dissolution due to contact with oral rinses or bleaching agents.

In the present paper, the values of the corrosion resistance exhibited by Ti-10Mo alloy suffer a direct effect of the hydrogen peroxide concentration. So, it is possible affirm that Er and Ev decreased with increasing concentration of hydrogen peroxide.

Results similar to those found in the present work were observed by Assis<sup>30</sup>, which investigated the corrosion resistance of titanium alloy containing 13% of neobium and 13% of zirconium in a hydrogen peroxide-containing environment. For this author, the formation of passive porous layer on the surface of the alloy allows to conclude that the resistance to corrosion can be explained by the type of layer or barrier that forms on the surface of the alloy.

Noguchi et al.<sup>31</sup> compared differences in discoloration and dissolution between commercially pure titanium alloy (c.p.Ti) and six titanium based alloys when immersed in hydrogen peroxide or fluoride solution. Their results showed that titanium associated with 20% chromium reached the lowest values for discoloration and dissolution.

Mohsen<sup>32</sup> studied the effect of bleaching agents (home use and dental office products) on the surface topography of three ceramometal dental alloys (gold, Ni-Cr, Co-Cr-Ti). Scanning electron microscopy revealed surface topographic alterations for all tested alloys in presence of both bleaching agents. The increased concentration of hydrogen peroxide led to increased surface roughness.

Takemoto et al.<sup>27</sup> investigated discoloration of commercially pure titanium, Ti-Pd, Ti-Al-V, Ti-Al-Nb, Ti-Ni, Ti-Cu and Ti-Cr alloys in acidic saline solutions with hydrogen peroxide. Their results suggest that discoloration in titanium alloys immersed in hydrogen peroxide-containing acidulated solutions is caused by an increase in the thickness of this oxide film, whereas discoloration of Ti-Ni is caused by corrosion.

Nakamura et al.<sup>33</sup> evaluated the corrosive effect of disinfection solution containing hydroxyl radicals generated by photolysis of  $H_2O_2$  on dental metals (Ti, Type 316L stainless steel, Ag-Pd-Cu-Au alloy and Co-Cr alloy) and observed that hydrogen peroxide can be applied to denture cleaning device without problematic metal corrosion unless the dentures contain Ti components.

Yokoyama et al.<sup>34</sup> suggested that localized corrosion of Ni-Ti alloy due to the synergistic effects of hydrogen peroxide and sodium chloride promotes fracture in vivo under stress.

Xie et al.<sup>35</sup> studied the influence of additives (K+, Ca<sup>2+</sup>, Na+, Mg<sup>2+</sup>, Cl-, HPO4<sup>2-</sup>, H<sub>2</sub>PO4<sup>2-</sup>) on corrosion

# CONCLUSION

Within the limits of this study, it may be concluded that values of Vickers hardness found for Ti-10Mo was higher than that of the c.p.Ti which suggests the better clinical performance of alloy. The corrosion values showed direct relation with the increase of the  $H_2O_2$  concentration.

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behavior of titanium in hydrogen peroxide solutions using spectrophotometer. They concluded that The results indicated that  $Ca^{2+}$  exhibited the highest inhibition to the titanium corrosion in hydrogen peroxide solutions, while  $H_2PO4^{2-}$  behaved as an accelerator to the corrosion.

The detrimental effect of bleaching agents on the passivation process of Ti-10Mo alloy observed in present study plays important influence on the dental device longevity. The corrosion can compromised the mechanical properties of titanium alloys and they might deleterious effects in tissues or cumulative effects in the body.

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#### **CONFLICTS OF INTERESTS**

The authors declare no conflicts of interests.

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